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# CERTIFICATE OF GRANT OF PATENT

In accordance with Section 24(2) of the Patents Act, 1977, it is hereby certified that a patent having the specification No 2282992 has been granted to Seiko Epson Corporation, in respect of an invention disclosed in an application for that patent having a date of filing of 23 August 1994 being an invention for "Ink jet recording head and method of manufacturing the same"

Dated this Twenty-sixth day of November 1997

Seiko Epson Corporation  
c/o J Miller & Co  
34 Bedford Row  
Holborn  
LONDON  
WC1R 4JH

P.R.S. HARTNACK  
Comptroller-General of Patents,  
Designs and Trade Marks.  
UNITED KINGDOM PATENT OFFICE





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(12) **UK Patent** (19) **GB** (11) **2 282 992** (13) **B**

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(54) Title of Invention

**Ink jet recording head and method of  
manufacturing the same**

(51) INT CL<sup>6</sup>: **B41J 2/045**

(21) Application No  
**9417126.1**

(22) Date of filing  
**23.08.1994**

(30) Priority Data

(31) **05207972**  
**05298477**

(32) **23.08.1993**  
**29.11.1993**

(33) **JP**

(43) Application published  
**26.04.1995**

(45) Patent published  
**26.11.1997**

(72) Inventor(s)  
**Keiichi Mukaiyama**  
**Kohei Kitahara**  
**Toshiki Usui**  
**Tomoaki Abe**

(73) Proprietor(s)  
**Seiko Epson Corporation**

**(Incorporated in Japan)**

**4-1 Nishi-shinjuku 2-chome**  
**Shinjuku-ku**  
**Tokyo**  
**Japan**

(74) Agent and/or  
Address for Service  
**J Miller & Co**  
**34 Bedford Row**  
**Holborn**  
**London**  
**WC1R 4JH**  
**United Kingdom**

(52) Domestic classification  
(Edition O)  
**B6F FLQ**

(56) Documents cited  
**EP0600743 A2**  
**EP0584823 A1**  
**EP0572230 A2**  
**US4680595 A**  
**US4424520 A**

(58) Field of search

As for published application  
2282992 A viz:  
UK CL(Edition M) **B6F FLQ**  
INT CL<sup>5</sup> **B41J 2/045 2/14**  
Online databases: **WPI,**  
**JAPIO.**  
updated as appropriate

1/12

FIG. 1

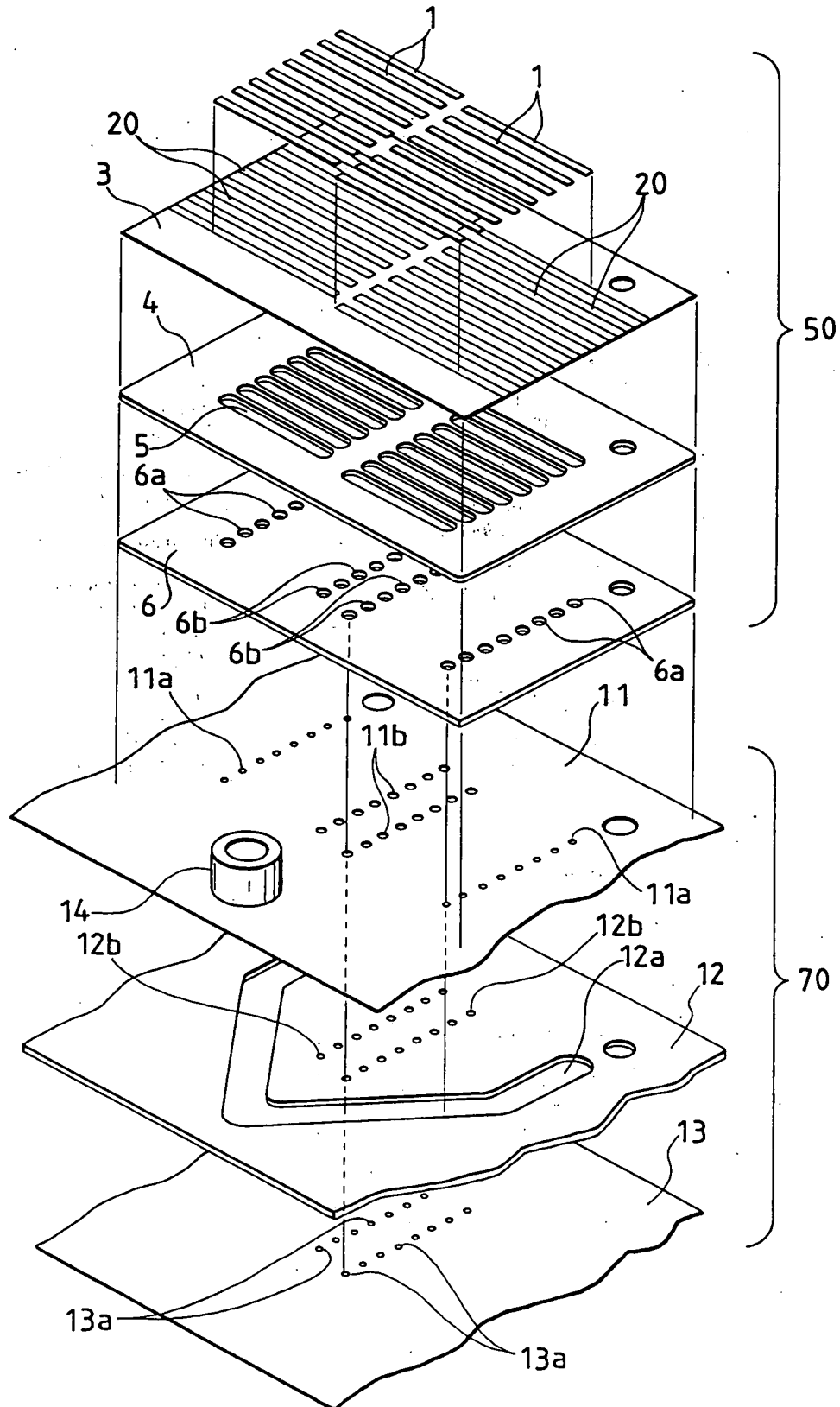


FIG. 2

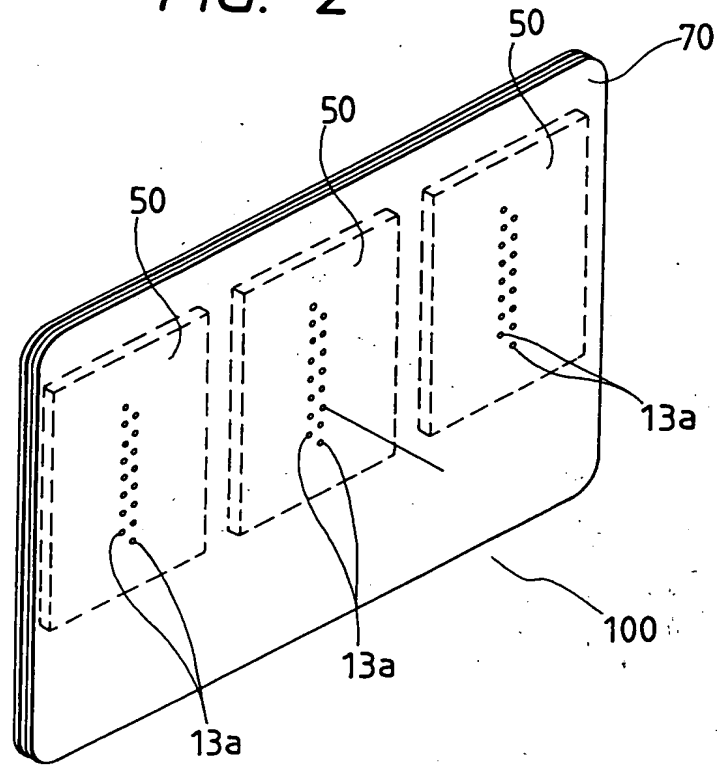


FIG. 3

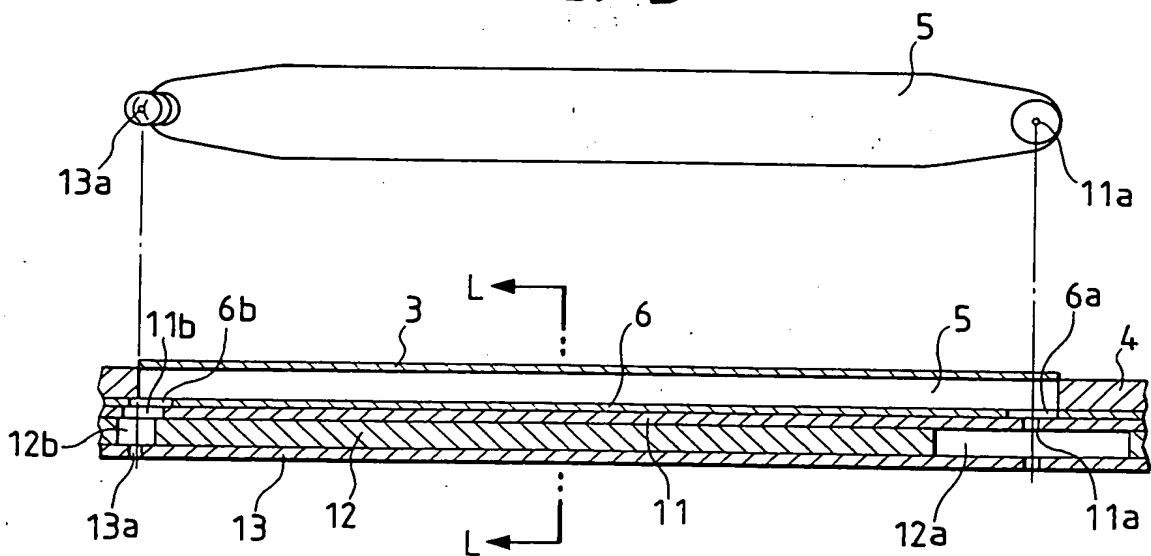


FIG. 4

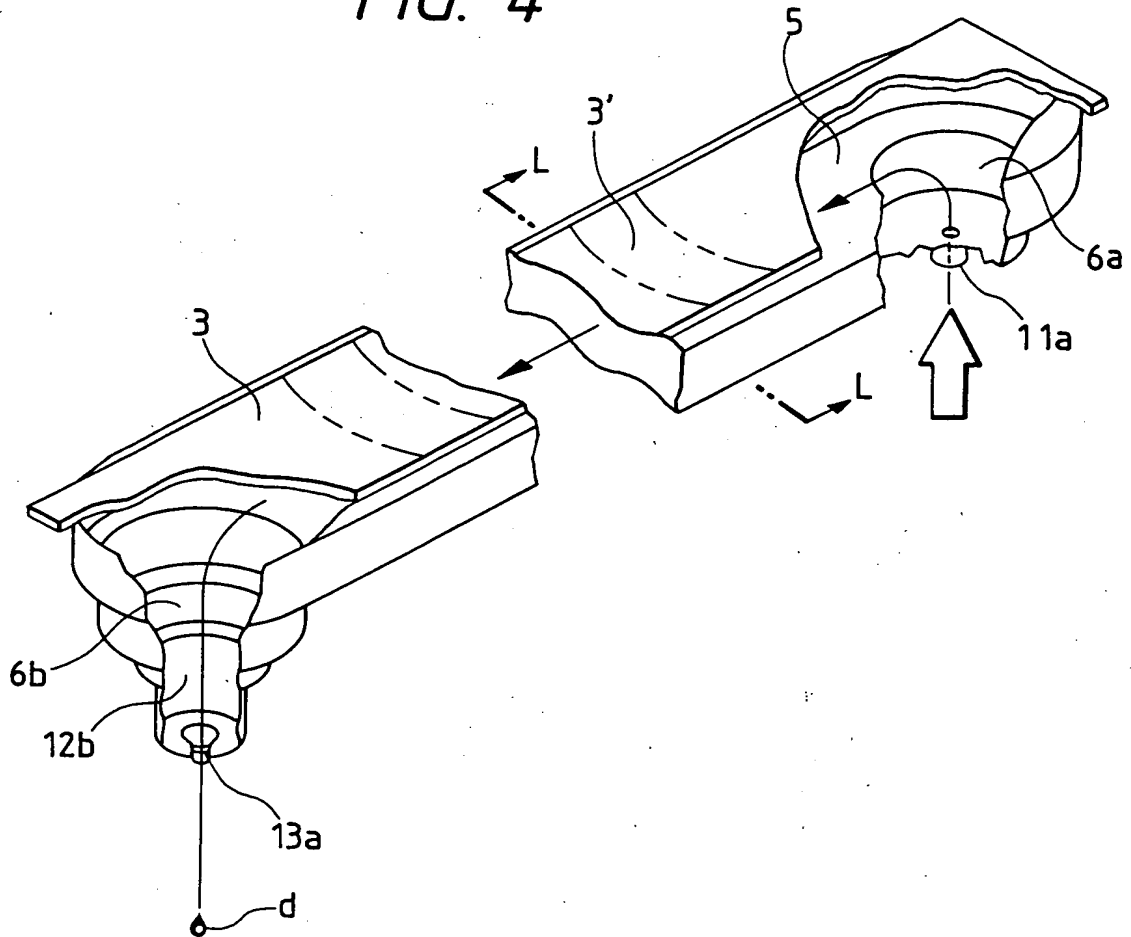


FIG. 5

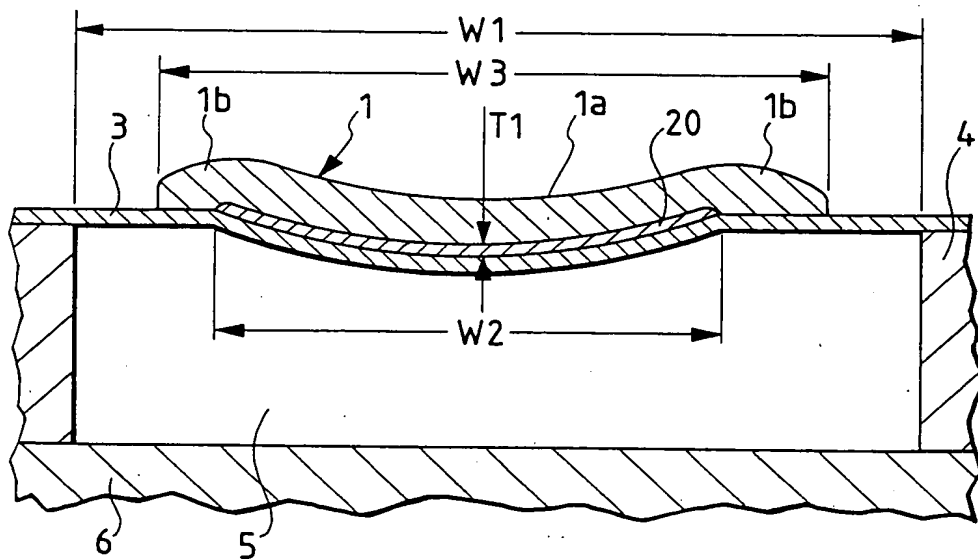


FIG. 6(a)

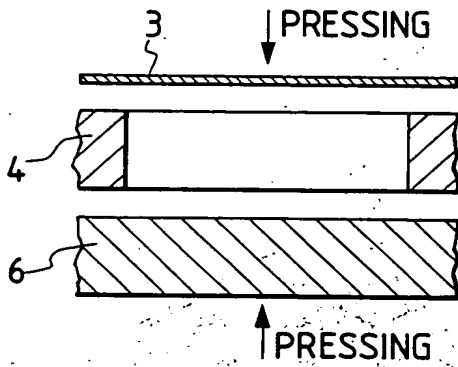
BAKING  
→

FIG. 6(b)

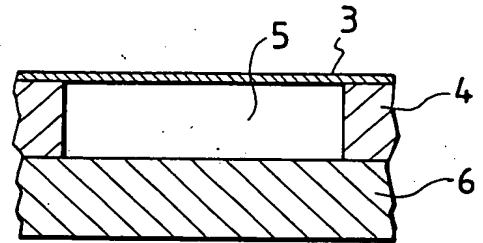


FIG. 6(c)

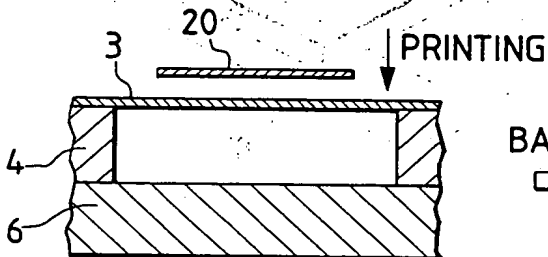
BAKING  
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FIG. 6(d)

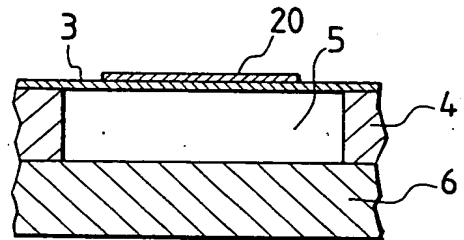


FIG. 6(e)

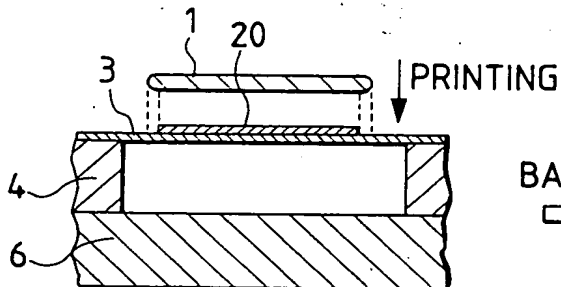
BAKING  
→

FIG. 6(f)

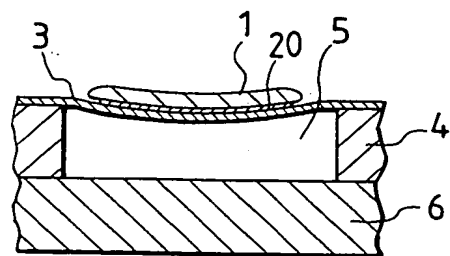


FIG. 7

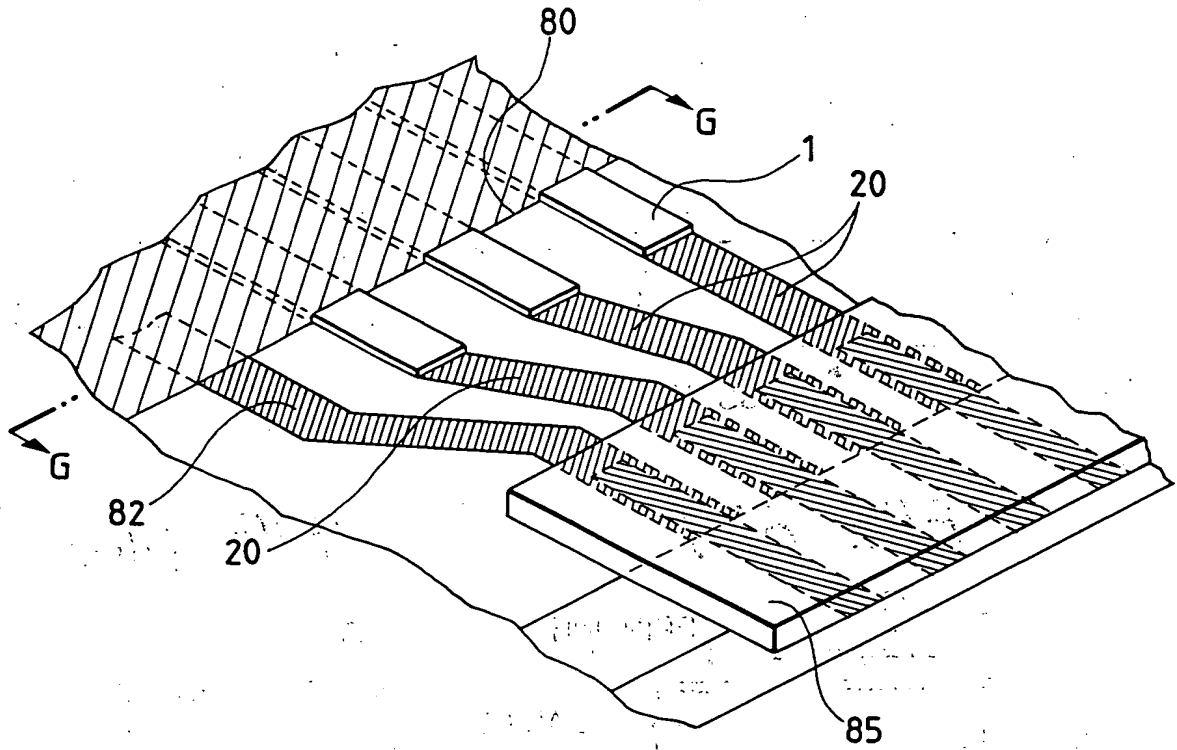


FIG. 8

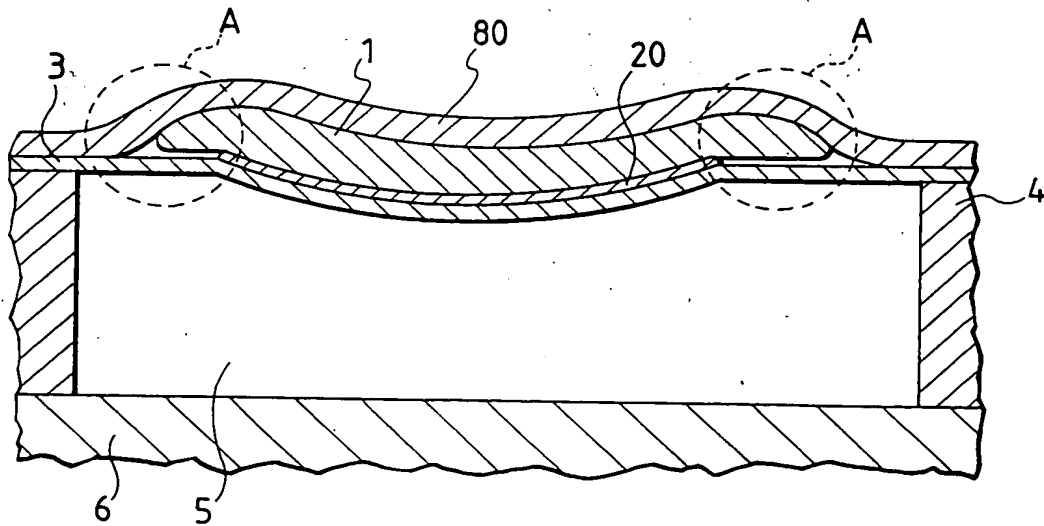


FIG. 9

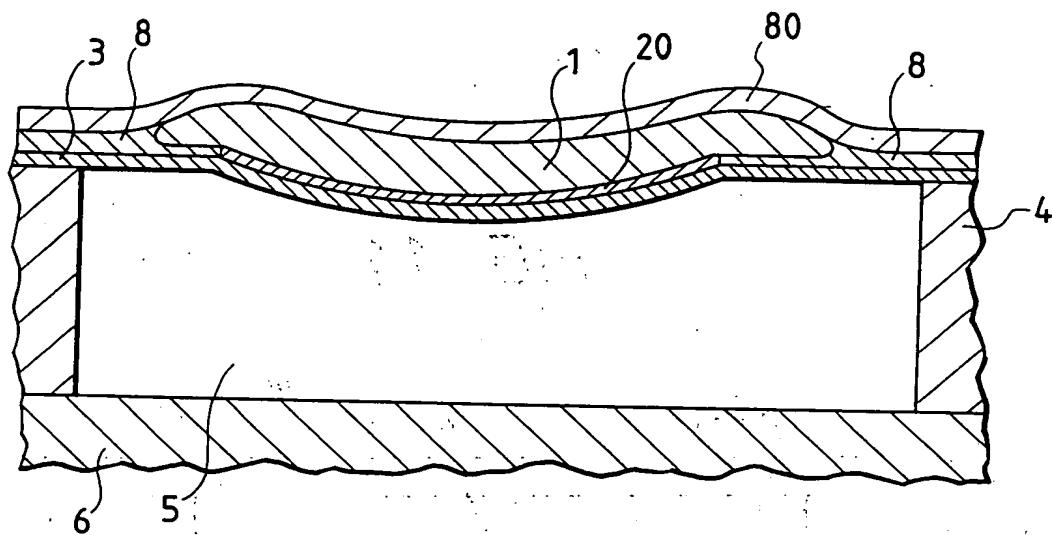


FIG. 10

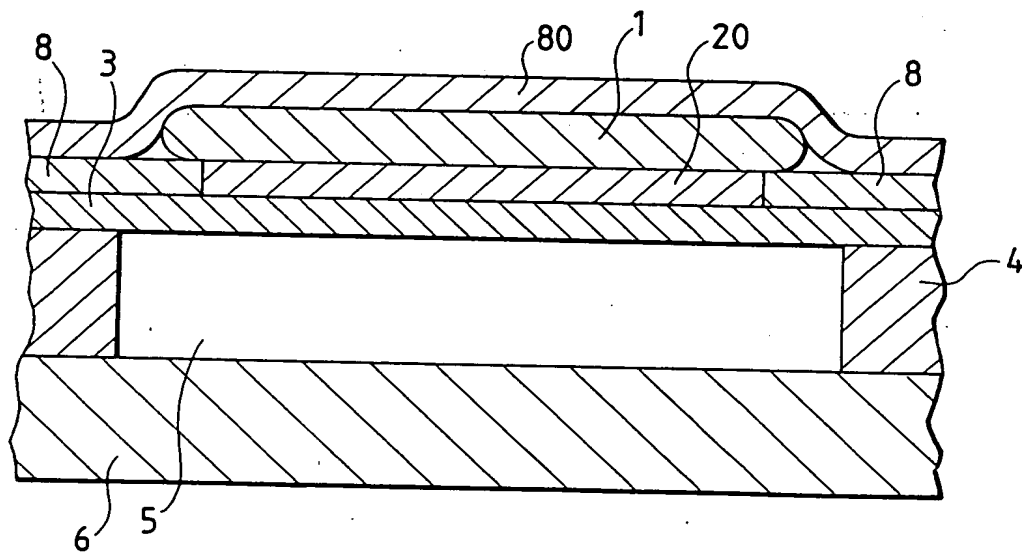


FIG. 11

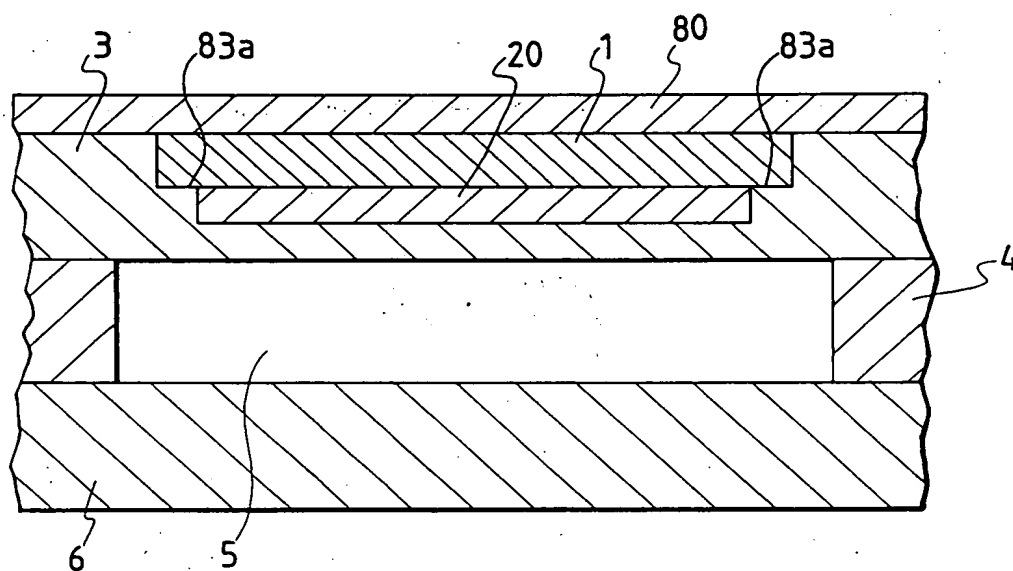


FIG. 12

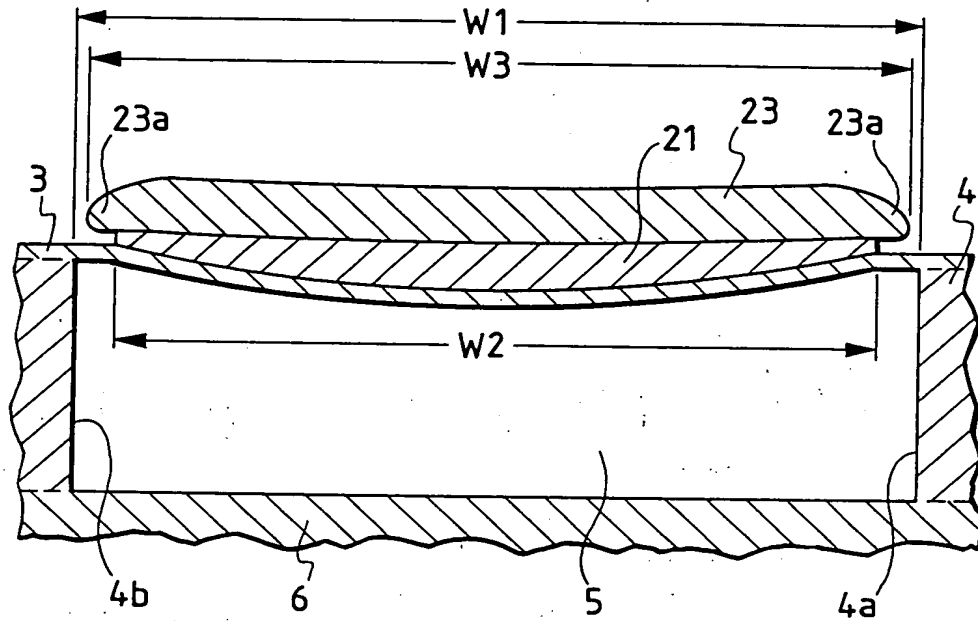


FIG. 13

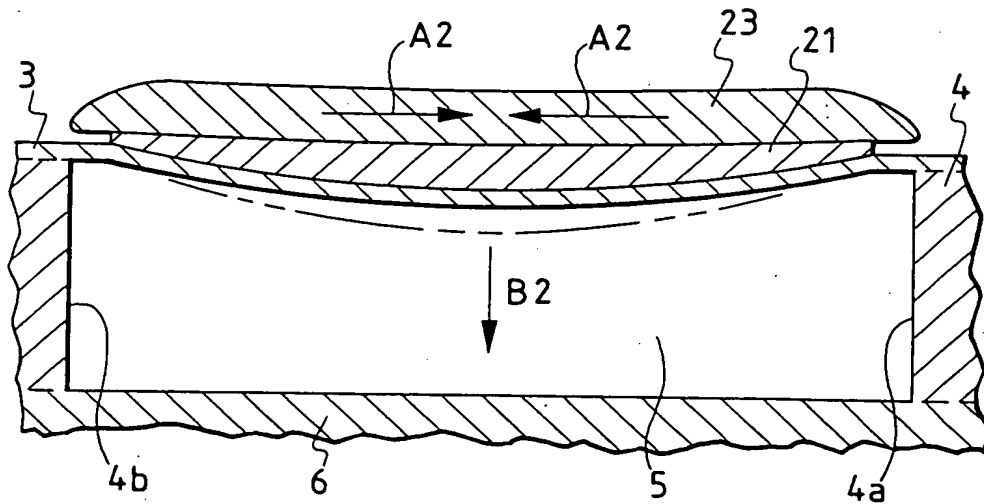


FIG. 14(a)

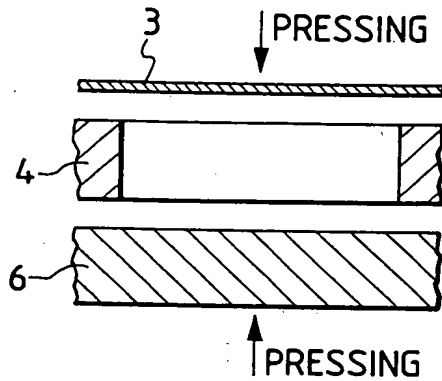


FIG. 14(b)

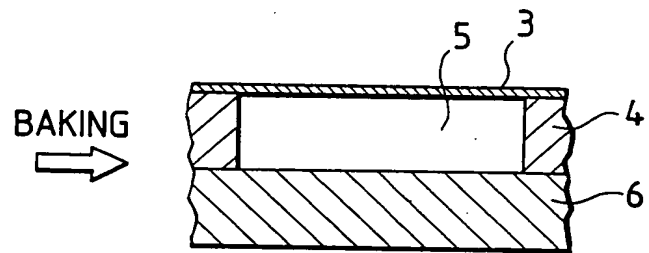


FIG. 14(c)

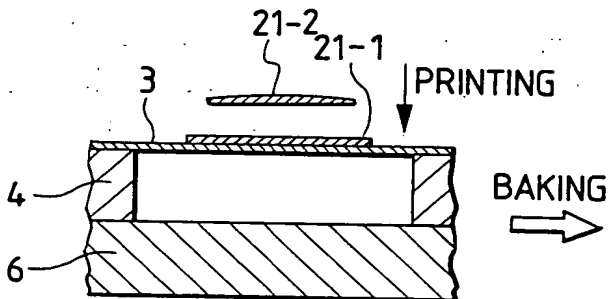


FIG. 14(d)

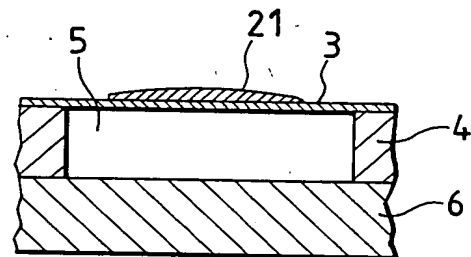


FIG. 14(e)

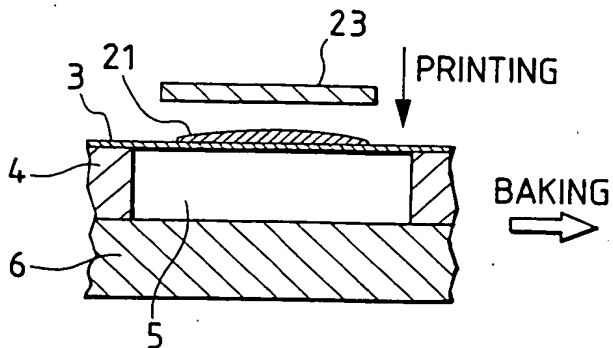


FIG. 14(f)

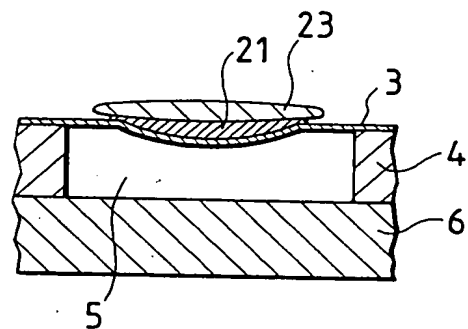


FIG. 15

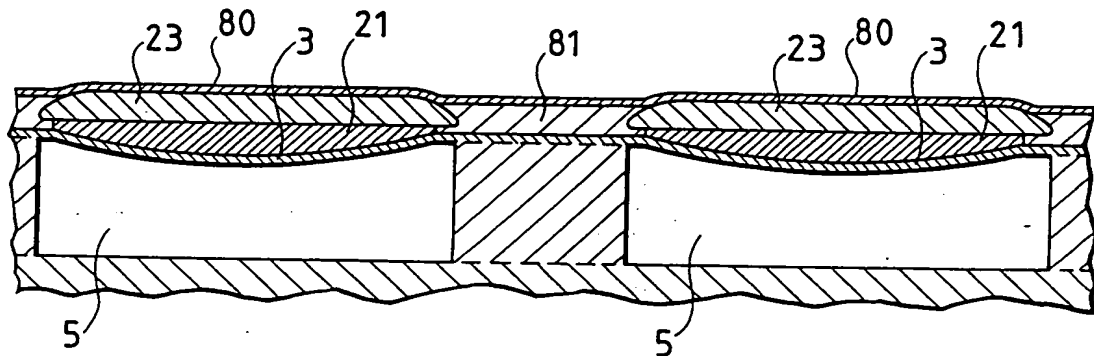


FIG. 16

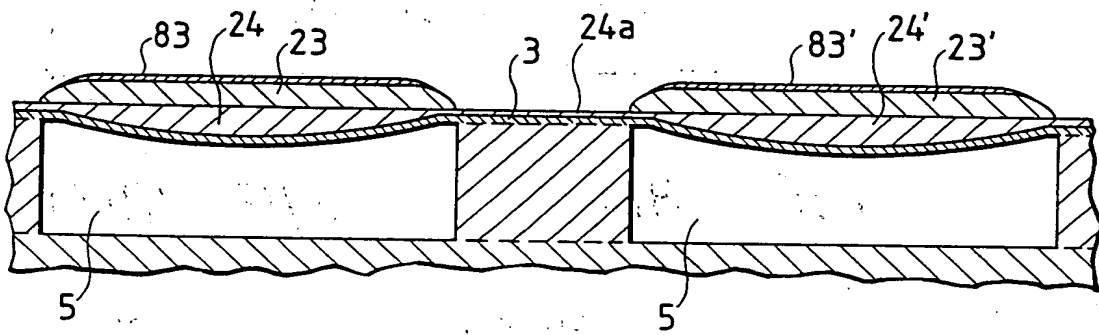


FIG. 17

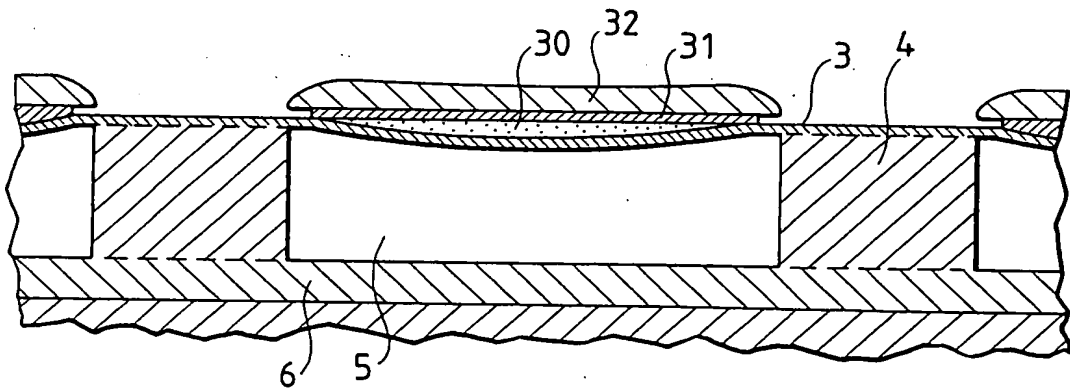


FIG. 18(a)

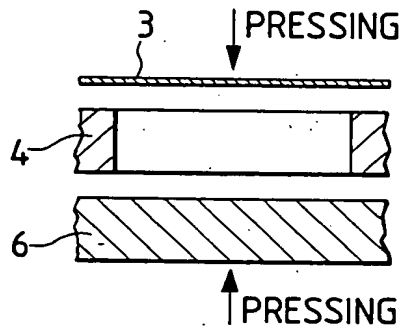


FIG. 18(b)

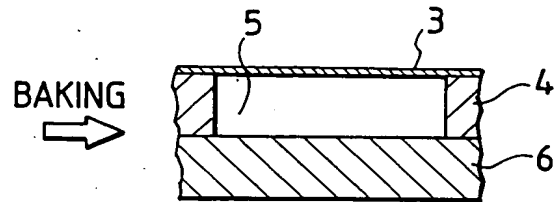


FIG. 18(c)

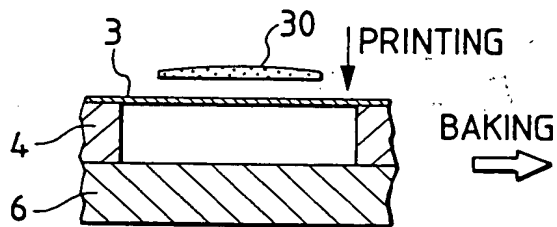


FIG. 18(d)

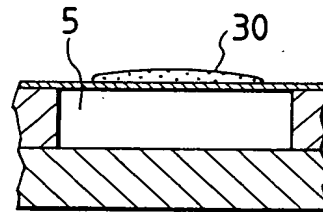


FIG. 18(e)

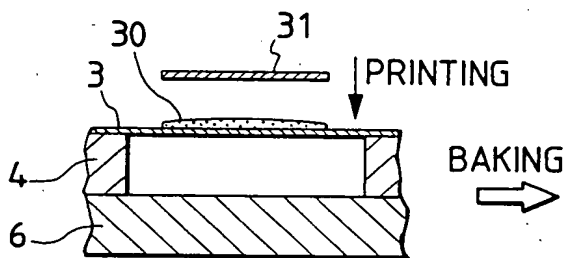


FIG. 18(f)

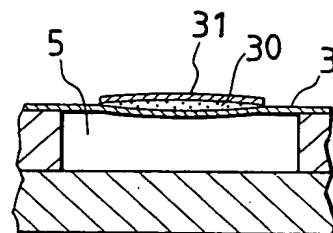


FIG. 18(g)

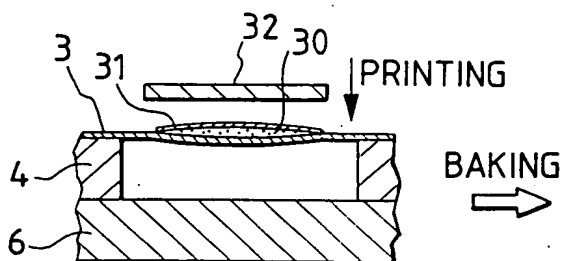


FIG. 18(h)

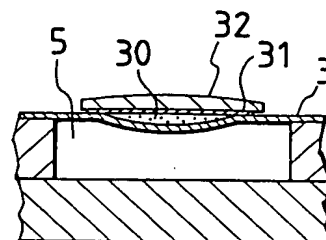


FIG. 19

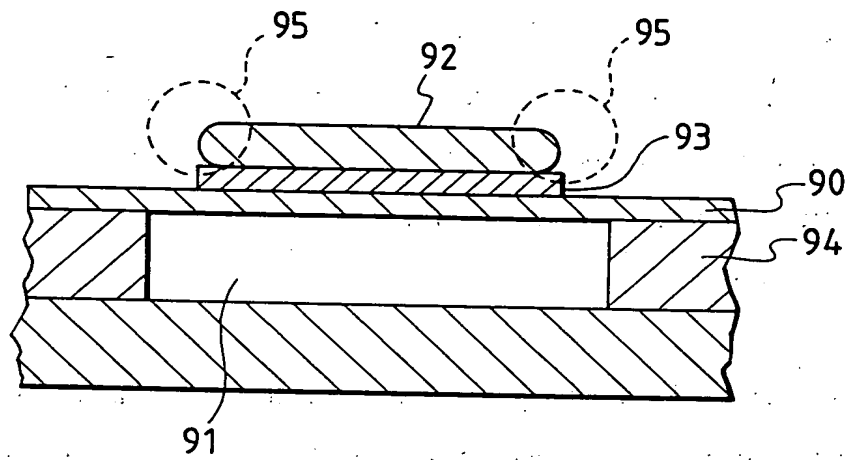
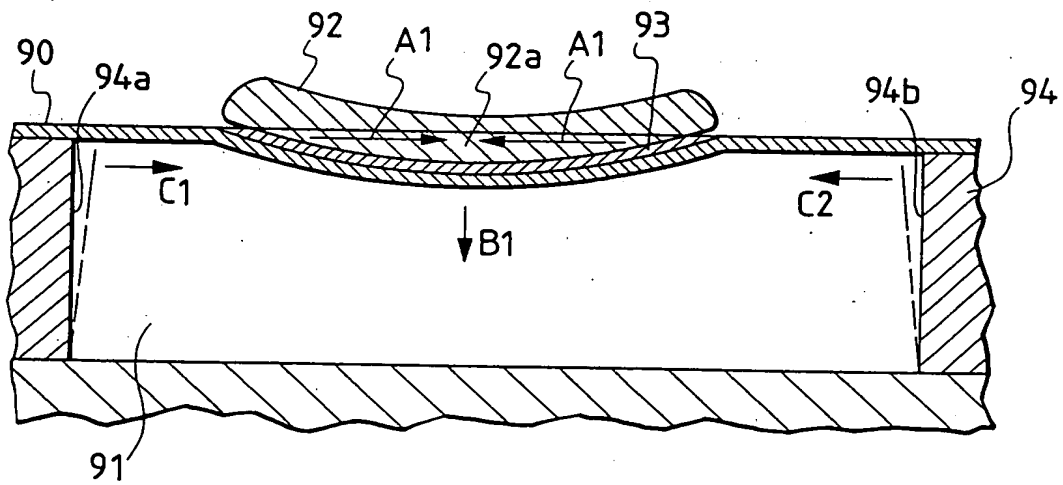


FIG. 20



**INK JET RECORDING HEAD  
AND  
METHOD OF MANUFACTURING THE SAME**

The invention relates to an on-demand ink jet recording head that forms characters and graphics on a recording medium with dots by expelling ink droplets thereto in accordance with input information. More particularly, the invention is directed to a structure having electrodes and piezoelectric vibrating elements formed on a surface of a vibrating plate as well as to a method of manufacturing such structure. The vibrating plate constitutes part of pressure producing chambers. The electrodes and the piezoelectric vibrating elements are formed integrally with the pressure producing chambers by baking.

Since an ink jet recording head has a structure such that an ink droplet is expelled by causing a piezoelectric element to be abutted against a small pressure producing chamber and increasing the pressure of ink within the pressure producing chamber by displacement of a vibrating plate, precision working and fabricating techniques are required in the manufacture thereof, which elevates the cost.

To overcome this problem, a structure shown in Figure 19 has been proposed attaching importance to the fact that the piezoelectric vibrating element, the vibrating plate constituting the pressure producing chamber, and the pressure producing chamber forming member can be made of ceramic. That is, a vibrating plate 90 formed by rolling a green sheet, which is a ceramic material, to a predetermined thickness and a pressure producing chamber forming member 94 having a pressure producing chamber 91 formed in advance by punching or machining with a laser beam a green sheet, which is also a ceramic material, are pressed and baked. Then, an electrode 93 is formed on the vibrating plate 90 and a piezoelectric vibrating element 92 is formed on the electrode 93 by baking.

Such an integrally baked ink jet recording head has the advantage of simple fabrication that involves only the steps of coating and baking a paste-like piezoelectric element by means of a printing technique. Further, since the pressure producing chamber forming member is integrated with the vibrating plate by baking, defective bonding such as observed in bonds formed by adhesives can be eliminated, which is an advantage in reliably preventing ink leakage.

However, the piezoelectric vibrating element, being such a small piece, is hard to uniformly coat to the corresponding drive electrode. Particularly, inconsistency in the bond of each piezoelectric vibrating element 92 with a peripheral edge 95 of the electrode 93 leads to inconsistency in the effective operation region between the piezoelectric vibrating elements, which in turn causes inconsistency in the ink expelling characteristic of each nozzle opening.

By the way, if the steps of depositing the electrode 93 on the surface of the vibrating plate 90, which is made of ceramic, and depositing the piezoelectric vibrating element 92 on the surface of the electrode 93 by baking are taken, the vibrating plate 90 generally flexes as shown in Figure 20. That is, the vibrating plate 90 flexes toward the pressure producing chamber 91 at a central portion of the pressure producing chamber 91 due to a difference in the rate of contraction between the piezoelectric vibrating element 92 and the electrode 93 at the time of baking. As a result, such a permanent deformation that a part 92a (the cross-hatched region in Figure 20) of the lower region of the piezoelectric vibrating element 92 projects toward the pressure producing chamber 91 tends to occur.

When the piezoelectric vibrating element 92 that has been deformed is caused to contract for expelling ink by applying a drive signal thereto, contracting forces in such horizontal directions indicated by arrows A1, A1 are generated as far as to the part 92a

of the lower region, thereby drawing in the horizontal directions the vibrating plate 90 that has already been flexed. As a result, a part of the contracting force draws walls 94a, 94b of the pressure producing chamber forming member 94 in directions indicated by arrows C1, C2 though the vibrating plate 90. Since the walls 94a, 94b of the pressure producing chamber forming member 94 are shared in common with the adjacent pressure producing chambers 91, the contraction of a single pressure producing chamber 91 is transmitted to other pressure producing chambers 91, causing crosstalk or cancelling out a force B1 that contributes to the ink expelling operation when adjacent piezoelectric vibrating elements 92, 92 are driven simultaneously, which impairs ink expelling efficiency.

That is, the displacement of the vibrating plate 90 in the case where a single piezoelectric element is driven is different from that in the case where a plurality of adjacent piezoelectric vibrating elements 92 are driven simultaneously, the difference being approximately twice. This causes differences in the ink droplet expelling speed and the amount of ink expelled, the differences being approximately 1.5 times.

A first object of the invention is to provide an ink jet recording head adapted to be manufactured by baking, the ink jet recording head being capable of providing consistent ink expelling performance among the nozzle openings by reliably bonding the piezoelectric vibrating elements to the electrodes formed on the vibrating plate and thereby making the effective operation regions of the piezoelectric vibrating elements uniform.

A second object of the invention is to provide an ink jet recording head adapted to be manufactured by baking, the ink jet recording head being capable of preventing crosstalk by controlling generation of divided forces that flex the walls of a pressure producing chamber and improving ink expelling efficiency independent of the deformation of the vibrating plate at the time of baking.

A third object of the invention is to propose a method of manufacturing the above-mentioned ink jet recording heads.

In a first aspect, this invention provides an ink jet recording head comprising:  
a plurality of chambers for retaining ink, each chamber having a length and width;

a vibrating plate disposed on a surface of the chambers;

a plurality of electrodes disposed on the vibrating plate, each electrode corresponding to a respective chamber;

a plurality of piezoelectric elements disposed on the electrodes, each piezoelectric element corresponding to a respective electrode and chamber

a common electrode disposed on the plurality of piezoelectric elements and providing an electric connection with each electrode at one end of the length of each chamber such that applying a drive signal across the common electrode and a selected electrode leads to flexing of the respective piezoelectric element which applies pressure to the respective chamber for expelling a drop of ink therefrom;

wherein at least the vibrating plate and chambers are formed from a ceramic and bonded together by baking,

each piezoelectric element is disposed to cover completely the width of the respective electrode,

and a peripheral edge of each piezoelectric vibrating element is formed as an overhang with respect to the electrode and is attached fixed to the vibrating plate via the electrode.

Since the width  $W3$  of the piezoelectric vibrating element formed on the vibrating plate is larger than the width of the electrode, the piezoelectric vibrating element can be bonded to the peripheral edges of the electrode reliably. Further, since the width  $W3$  is

smaller than the width  $W1$  of the pressure producing chamber, the piezoelectric vibrating element is free from interference from the non contracting regions.

Figure 1 is an exploded perspective view showing an ink jet recording head, which is an embodiment of the invention;

Figure 2 is a perspective view outlining the ink jet recording head of the invention;

Figure 3 is an enlarged sectional view showing the shape of the upper surface of a pressure producing chamber and the longitudinal section thereof in the ink jet recording head;

Figure 4 is a partially sectional perspective view showing the structure of the pressure producing chamber;

Figure 5 is a diagram showing the structure having a drive electrode and a piezoelectric vibrating element, which is the feature of the invention, in section taken along a line L-L of Figure 4;

Figures 6(a) to (f) are diagrams showing a method of manufacturing a pressure producing unit used in the ink jet recording head of the invention;

Figure 7 is a perspective view showing the structure of the surface of the vibrating plate;

Figures 8 to 11 are sectional views respectively showing other embodiments of the pressure producing units used in the ink jet recording head of the invention;

Figure 12 is a sectional view showing another embodiment of the pressure producing unit used in the ink jet recording head of the invention;

Figure 13 is a diagram showing forces generated at the time the piezoelectric vibrating element contracts in the pressure producing unit shown in Figure 12;

Figures 14(a) to (f) are diagrams showing a method of manufacturing the pressure producing unit shown in Figure 12;

Figures 15 to 17 are sectional views respectively showing other embodiments of the pressure producing units used in the ink jet recording head of the invention;

Figures 18(a) to (h) are diagrams showing a method of manufacturing the pressure producing unit shown in Figure 17; and

Figures 19 and 20 are sectional views respectively showing relationships between the drive electrode and the piezoelectric vibrating element in a conventional pressure producing unit in which the drive electrode and the piezoelectric vibrating element are manufactured integrally by baking.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The invention will now be described in detail with reference to the embodiments shown in the drawings.

Figure 1 shows an ink jet recording head, which is an embodiment of the invention, to which the electrode structure of the invention is applied. In Figure 1 reference numeral 3 denotes a vibrating plate made of a material, at least the surface of which is electrically insulating, more preferably, of ceramic. On the surface of the vibrating plate 3 are drive electrodes 20, which will be described later. The drive electrodes are arranged so as to correspond to a plurality of rows of pressure producing chambers 5, 5, 5, . . . (two (2) rows in this embodiment). Reference numeral 1 denotes a piezoelectric vibrating element that is made of ceramic and has a piezoelectric property. The piezoelectric vibrating elements 1 flex toward the vibrating plate 3 through the drive electrodes 20, 20, 20 . . . so that the back surfaces thereof come in contact with the drive electrodes 20, 20, 20 . . .

Reference numeral 4 denotes a pressure producing chamber forming member, which is made of a plate that is so thick as to form the pressure producing chambers 5, 5, 5 . . ., more preferably, of a ceramic plate, by boring through holes therein. Reference numeral 6 denotes a pressure producing chamber forming cover member, which serves to seal the other surface of the pressure producing chambers 5 of the pressure producing chamber forming member 4. At positions corresponding to the vicinity of both ends of the pressure producing chambers 5 are introducing holes 6a, 6a, 6a . . . and introducing holes 6b, 6b, 6b . . . The introducing holes 6a, 6a, 6a . . . communicate with a common ink chamber 12a, which will be described later, and the introducing holes 6b, 6b, 6b . . . communicate with nozzle openings 13a, 13a, 13a . . .

The vibrating plate 3 having both the piezoelectric vibrating elements 1 and the drive electrodes 20, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6 are collected into a small group having two

(2) rows of nozzle openings, all these members being preferably made of ceramic, and integrated by baking into a pressure producing unit 50.

Reference numeral 11 denotes an ink supply section forming member. The ink supply section forming member 11 includes: an ink introducing inlet 14 that supplies ink into the ink chamber 12a that is shared in common while connected to a flow path from a not shown ink tank; introducing through holes 11a that connect the pressure producing chambers 5 to the common ink chamber 12a; and introducing through holes 11b that connect the pressure producing chambers 5 to the nozzle openings 13a.

Reference numeral 12 denotes a reservoir forming member that forms the common ink chamber 12a. In this embodiment the common ink chamber 12a is formed by a through hole that is substantially V-shaped, and is connected to the respective pressure producing chambers 5 through the introducing through holes 6a of the above-mentioned pressure producing chamber forming cover member 6 and the introducing through holes 11a of the ink supply section forming member 11. Introducing through holes 12b that connect the pressure producing chambers 5 to the nozzle openings 13a are formed at a central portion of the reservoir forming member 12.

Reference numeral 13 denotes a nozzle forming member. The nozzle forming member 13 is connected to the pressure producing chambers 5 through the introducing through holes 6b, 11b, 12b, and also performs the function of sealing the other side of the common ink chamber 12 of the reservoir forming member 12.

The ink supply section forming member 11 and the nozzle forming member 13 are formed by press working or etching a rustproof steel sheet. These members may be made of at least one material selected from the group consisting of other metals, ceramics, glass, silicon, and plastics. The method of working the respective members includes: press working, etching, electroforming, and laser beam machining. At any rate, a material having a relatively high Young's modulus is selected for the ink supply section forming member 11 and the nozzle forming member 13.

On the other hand, the reservoir forming member 12 may be made of not only the above-mentioned metals, ceramics, glass, and silicon, but also a plastic - or film-like

adhesive or paste-like adhesive such as polyimide, polyamide, polyester, polyethylene, polypropylene, polyvinyl chloride, and polyvinylidene chloride may be used since not so high a rigidity is required for the reservoir forming member 12. When the plastic - or film-like adhesive is used, the reservoir forming member 12 is formed by injection moulding or press working. When the paste-like adhesive is used, the reservoir forming member 12 is formed by screen printing or transfer printing.

The ink supply section forming member 11, the reservoir forming member 12, and the nozzle forming member 13 are formed into a flow path unit 70 that has the function of fixing a plurality of pressure producing units 50.

A method of bonding these members into a flow path unit is as follows. If the reservoir forming member 12 itself has no adhesion, the film-like adhesive or the paste-like adhesive is used, and the ink supply section forming member 11, the adhesive, the reservoir forming member 12, the adhesive, and the nozzle forming member 13 are laminated one upon another in this order using a not shown positioning jig, and thermocompressed or compressed. On the other hand, if the reservoir forming member 12 itself has adhesion, the ink supply section forming member 11, the reservoir forming member 12, and the nozzle forming member 13 are laminated one upon another in this order and similarly thermocompressed or compressed.

As a result, a single sheet of flow path unit 70 as shown in Figure 2 has a plurality of pressure producing units 50, namely, three (3) pressure producing units 50, 50, 50 in this particular embodiment, collectively fixed thereto by the adhesive, thermodeposition film, or the like to form an ink jet recording head.

The thus formed pressure producing chambers 5 of the ink jet recording head are substantially rectangular, slender chambers such as shown in Figure 3. The nozzle opening 13a communicates with one end of each pressure producing chamber 5, and the common ink chamber 12a communicates with the other end thereof. As shown in Figure 4, with the piezoelectric vibrating element 1 vibrating by flexion, the vibrating plate 3 is deformed so that the vibrating plate 3 projects toward the pressure producing chamber 5

increases to jet an ink droplet "d" from the nozzle opening 13a and thereby form a dot on a recording sheet. Upon return of the piezoelectric vibrating element 1 to the original conditions, the ink flows from the common ink chamber 12a via the introducing through hole 11a. As a result, a stream of ink in such a longitudinal direction as indicated by the arrows in Figure 4 is produced within the pressure producing chamber 5.

Figure 5 shows in section a structure of the thus constructed ink jet recording head in the vicinity of the pressure producing chamber as viewed in a direction orthogonal to the stream of ink within the pressure producing chamber 5, or as taken along a line L-L of Figure 4. In Figure 5 reference numeral 20 denotes the drive electrode formed on the surface of the vibrating plate 3. The width W2 of the drive electrode 20 is slightly smaller than the width W1 of the pressure producing chamber 5, and the drive electrode 20 is formed so as to have a length so that one end thereof reaches an end portion of the vibrating plate 3 from the vicinity of the nozzle opening 13a of the pressure producing chamber 5, and the other end thereof serves also as the connecting terminal with an outer electrode.

Reference numeral 1 denotes the piezoelectric vibrating element, whose width W3 is larger than the width W2 of the drive electrode 20 and smaller than the width W1 of the pressure producing chamber 5. Having such a length that the front end thereof on the nozzle opening side covers the drive electrode 20 and the rear end thereof reaches the vicinity of the rear end of the pressure producing chamber 5, the piezoelectric vibrating element 1 is also formed so as to cover completely the region of the drive electrode 20 confronting the pressure producing chamber 5.

By forming the piezoelectric vibrating element 1 so as to cover the region of the drive electrode 20 confronting the pressure producing chamber 5, the region of the drive electrode 20 confronting the pressure producing chamber 5 can be covered completely by the piezoelectric vibrating element 1 even if the piezoelectric vibrating element 1 is subjected to slight displacement or sized inconsistently when formed. This prevents short circuit with a common electrode 80 (Figure 7) on the other pole which is formed on the surface of the piezoelectric vibrating element 1.

In the case where the piezoelectric vibrating element 1 is formed by coating or bonding the green sheet, which is a piezoelectric material, to the drive electrode 20 and baking the green sheet together with the vibrating plate 3 and the drive electrode 20, the piezoelectric vibrating element 1 covers the drive electrode 20 completely and has the peripheral edge portion 1b bonded to the drive electrode 20 reliably against contraction of the piezoelectric vibrating element 1 and flexion of the vibrating plate 3 during the baking process. Therefore, not only displacement by flexion of the piezoelectric vibrating element 1 can be transmitted to the vibrating plate 3 reliably, but also fatal damage such as partial flaking or the like can be prevented owing to the reliable bondage between the piezoelectric vibrating element 1 and the vibrating plate 3.

The area of the drive electrode 20 itself is used as the effective operation region of the piezoelectric vibrating element 1 since the piezoelectric vibrating element 1 is deposited so as to cover the drive electrode 20 in this invention. As a result, a piezoelectric vibrating element 1 that has an optimal effective operation region with respect to the pressure producing chamber 5 can be formed with ease by adjusting the size of the drive electrode 20 that is thin and can be formed highly accurately with ease. Such adjustment is easier to make than the adjustment of the size of the piezoelectric vibrating element 1 that is comparatively thick.

In addition, to improve displacement efficiency of the vibrating plate 3, i.e., the ratio of the applied electric energy to the ink removing volume, it is ideal to adjust the ratio of the width W1 of the pressure producing chamber 5 to the width W2 of the drive electrode 20,  $W2/W1$ , to 0.9. However, such ratio may be set to a value between 0.8 and 0.9 considering errors and variations in the manufacturing process.

Specifically, a drive electrode 20, whose width W2 is 340  $\mu\text{m}$  and whose thickness is 5  $\mu\text{m}$  that is a thickness to allow electric conduction to be ensured with respect to a pressure producing chamber having a width W1 of 420  $\mu\text{m}$ , is formed, and then a piezoelectric vibrating element 1, whose width W3 is 380  $\mu\text{m}$  and whose thickness is 30  $\mu\text{m}$ , is formed on the surface of the drive electrode 20.

A method of manufacturing the thus constructed ink jet recording head will be described next.

Figures 6(a) to (f) are diagrams showing a method of manufacturing the above-mentioned pressure producing unit 50, the method being an embodiment of the invention. The vibrating plate 3, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6 are formed of green sheets, each green sheet being a ceramic material, i.e., a clay-like sheet, and the pressure producing chamber forming member 4 having windows formed at regions designed to serve as the pressure producing chambers 5 by punching; and pressure is applied to the green sheets with these members half-solidified so that these members are integrated with one another, in Figure 6(a). Then, the thus processed body is baked at temperatures ranging from 800 to 1500°C, in Figure 6(b). The ceramic material generally consists essentially of one kind or more of compound selected from the group consisting of aluminum oxide, zirconium oxide, magnesium oxide, aluminum nitride, and silicon nitride.

When the vibrating plate 3, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6 have been integrated, a pattern of the drive electrode 20 having an optimal width with respect to the corresponding pressure producing chamber 5 is formed by coating or printing an electrically conducting material to a region corresponding to the pressure producing chamber 5 of the vibrating plate 3 so that the ratio of the width  $W_2$  of the drive electrode 20 to the width  $W_1$  of the pressure producing chamber 5,  $W_2/W_1$ , is set to a value between 0.8 and 0.9, in Figure 6(c). The electrically conducting material consists essentially of one kind or more of alloy selected from the group consisting of platinum, palladium, silver-palladium, silver-platinum, and platinum-palladium.

After the pattern of the drive electrode 20 has been half-solidified on the vibrating plate 3, the whole body is baked at a temperature suitable for baking the electrically conducting material, in Figure 6(d).

Then, the piezoelectric vibrating element 1 is formed on the surface of the drive electrode 20 by coating or printing a green sheet consisting of a piezoelectric material so that the width W3 of the piezoelectric vibrating element 1 is larger than the width W2 of the drive electrode 20 formed on the surface of the vibrating plate 3 and smaller than the width W1 of the pressure producing chamber 5, in Figure 6(e). The piezoelectric material consists essentially of lead zirconate titanate, lead magnesium-niobate, lead nickel-niobate, lead zinc-niobate, lead manganese-niobate, lead antimony-stannate, or lead titanate.

When the green sheet, which is a piezoelectric material and which has been formed so as to slightly overhang the drive electrode 20, has been half-solidified in this way, the whole body is baked at a temperature suitable for baking the piezoelectric material, Figure 6(f). In this baking process the central portion 1a of the piezoelectric vibrating element 1 may, in some cases, flex so as to project toward the pressure producing chamber 5 as shown in Figure 5 due to the rate of contraction of the piezoelectric vibrating element 1 at the time of baking being larger than that of the drive electrode 20 and due to contraction of the portions of the piezoelectric vibrating element 1 overhanging the drive electrode 20 being larger than contraction of the piezoelectric vibrating element 1 on the drive electrode 20.

However, this type of piezoelectric vibrating element 1 is advantageous in preventing itself from being partially flaked and completely flaked from the drive electrode 20 since the piezoelectric vibrating element 1 is bonded to the drive electrode 20 with the peripheral portions 1b thereof overhanging the vibrating plate 3 while extending from the drive electrode 20.

As all the baking processes have been completed in this way, the piezoelectric vibrating elements 1, 1, 1 and the common electrode 80 arranged over the piezoelectric vibrating elements are deposited over an entire region confronting the pressure producing chambers 5 by forming an electrically conducting film by means of a film forming method such as selective vapor deposition or sputtering while using an electrically conducting material, eg., nickel or copper, with a mask as shown in Figure 7. The

common electrode 80 is connected to an external device by a cable 85 together with the drive electrodes 20, 20, 20 . . . through a lead electrode 82.

As a result, an ink droplet can be expelled from the nozzle opening 13a by flexing the piezoelectric vibrating element 1 while applying a drive signal across the common electrode 80 and the drive electrode 20 positioned at the pressure producing chamber 5 from which the ink droplet is to be expelled.

The peripheral edge portions 1b, 1b of the piezoelectric vibrating element 1, i.e., the portions overhanging from the peripheral edge portions of the drive electrode 20 are bonded to the vibrating plate 3 in the above-mentioned embodiment. As shown in Figure 8 the peripheral edges A, A of the piezoelectric vibrating element 1 are baked so as to overhang the drive electrode 20 by, eg., preparing a slightly solidier green sheet, so that the effective operation region of the piezoelectric vibrating element 1 can be limited to the width of the drive electrode 20 itself with the reliable bondage between the piezoelectric vibrating element 1 and the drive electrode 20 well maintained.

As a result, all the pressure producing chambers 5 can be driven under a consistent condition, free from inconsistency in the vibrating characteristic caused by inconsistency in the size of the piezoelectric vibrating element 1, the size thereof tending to be inconsistent in the widthwise direction.

If necessary, an electrically insulating layer 8, which is thinner than the piezoelectric vibrating element 1, is formed at a region of the vibrating plate 3 where no piezoelectric vibrating element 1 is formed as shown in Figure 9, and the common electrode 80 is deposited thereon, so that not only generation of crosstalk due to signal leakage can be prevented by ensuring electric insulation between the adjacent drive electrodes 20, but also breakage of the common electrode 80 at the ends of the piezoelectric vibrating element 1 can be prevented by making the step between piezoelectric vibrating element 1 and the vibrating plate 3 small.

Figure 10 shows an embodiment in which the insulating material layer 8 and the drive electrode 20 are formed on a single sheet so that the insulating material layer 8 surrounds the drive electrode 20 and so that the upper surfaces of both the insulating

material layer 8 and the drive electrode 20 are flush with each other. According to this embodiment, electrically caused crosstalk can be prevented by electrically insulating the drive electrode 20 reliably, and the common electrode 80 can be formed more reliably.

Figure 11 shows still another embodiment of the invention. A slightly thicker ceramic material, which will become the vibrating plate 3, is prepared. In addition, a recessed portion 83 having a step 83a for accommodating the drive electrode 20 and the piezoelectric vibrating element 1 is formed at a central portion of each pressure producing chamber 5, so that the drive electrode 20 and the piezoelectric vibrating element 1 that is slightly wider than the drive electrode 20 are accommodated on the bottom thereof and on the top thereof, respectively, with the surface of the piezoelectric vibrating element 1 being as high as other regions of the vibrating plate 3 which have nothing to do with displacement. According to this embodiment, not only both mechanically caused crosstalk and electrically caused crosstalk due to signal leakage can be prevented by sufficiently reinforcing the regions not having to do with the displacement of the pressure producing chamber 5, but also reliability can be improved by forming the common electrode 80 so as to be stepless.

Figure 12 shows an ink jet recording head, which is still another embodiment of the invention. This embodiment is designed to overcome the second problem, i.e., reduction in ink expelling efficiency caused by the deformation of the piezoelectric vibrating element and the vibrating plate at the time of baking, as well as crosstalk. Figure 12 shows the embodiment in terms of the structure of a section taken in a direction orthogonal to the stream of ink within the pressure producing chamber 5, i.e., along a line L-L of Figure 4.

In Figure 12 reference numeral 21 denotes a drive electrode formed on a surface of the vibrating plate 3. This drive electrode 21 is formed so that the width thereof  $W_2$  is slightly smaller than the width  $W_1$  of the pressure producing chamber 5. The drive electrode 21 is arcuate in section so that the central portion thereof in the longitudinal direction of the pressure producing chamber 5, i.e., on a line connecting the nozzle opening to the common ink chamber is projected toward the pressure producing chamber

5 and the top thereof that is in contact with a piezoelectric vibrating element 23 is substantially horizontal.

While the drive electrode 20 in the above-mentioned embodiment has the uniform thickness of about 5  $\mu\text{m}$  attaching importance only to the electric property, the drive electrode 21 according to this embodiment sets the thickness of the central portion thereof to values ranging from 15 to 30  $\mu\text{m}$  with flexion at the time of baking being taken in consideration, although the thickness of the peripheral edge portions is set to about 5  $\mu\text{m}$  so that the electric property can be maintained.

Reference numeral 23 denotes the piezoelectric vibrating element. The width  $W_3$  of this piezoelectric vibrating element 23 is larger than the width  $W_2$  of the drive electrode 21 and smaller than the width  $W_1$  of the pressure producing chamber 5. Having such a length that the front end thereof on the nozzle opening side covers the drive electrode 21 and the rear end thereof reaches the vicinity of the rear end of the pressure producing chamber 5, the piezoelectric vibrating element 23 is formed so as to cover completely the region of the drive electrode 21 corresponding to the pressure producing chamber 5. The peripheral edge portions 23a, 23a of the piezoelectric vibrating element 23 are formed so as to overhang the drive electrode 21 in a manner similar to those in the above-mentioned embodiment.

According to this embodiment, the sectional structure of the drive electrode 21 is selected so as to fill the space formed by the above-mentioned flexion of the vibrating plate 3, the flexion being caused by the difference in the rate of contraction between the piezoelectric vibrating element 23 and the drive electrode 21 at the time of baking. Therefore, the upper surface of the drive electrode 21 is kept substantially horizontal after the baking, thereby making the piezoelectric vibrating element 23 formed on the drive electrode 21 flat also.

As a result, when the piezoelectric vibrating element 23 is contracted by applying a drive signal thereto, horizontally drawing forces  $A_2$ ,  $A_2$  are generated on the surface higher than the vibrating plate 3 as shown in Figure 13. Although such forces are transformed into a force  $B_2$  that flexes the vibrating plate 3 toward the pressure

producing chamber 5, these forces do not draw walls 4a, 4b that define the pressure producing chamber 5 toward the pressure producing chamber 5. Consequently, not only an ink droplet is expelled at a high efficiency, but also generation of crosstalk is controlled to an extremely small degree.

It goes without saying that, by forming the piezoelectric vibrating element 23 so as to cover the region of the drive electrode 21 confronting the pressure producing chamber 5, the region of the drive electrode 20 confronting the pressure producing chamber 5 can be covered completely by the piezoelectric vibrating element 23 even if slight displacement or inconsistency in size are present with the drive electrode 21 and the piezoelectric vibrating element 23. This prevents short-circuiting with a common electrode 80 on the other pole which is formed on the surface of the piezoelectric vibrating element 23.

In the case where the piezoelectric vibrating element 23 is formed by coating or bonding a green sheet, which is a piezoelectric material, to the drive electrode 21 and baking the green sheet together with the vibrating plate 3 and the drive electrode 21, the piezoelectric vibrating element 23 covers the drive electrode 21 completely and has peripheral edge portions 23a, 23a bonded to the drive electrode 21 reliably against the above-mentioned flexion of the vibrating plate 3 caused by the difference in the rate of contraction between the piezoelectric vibrating element 23 and the drive electrodes 21 at the time of baking. Therefore, not only displacement by flexion of the piezoelectric vibrating element 23 can be transmitted to the vibrating plate 3 reliably, but also fatal damage such as partial flaking or the like can be prevented owing to the reliable bondage between the piezoelectric vibrating element 23 and the vibrating plate 3.

Specifically, a drive electrode 21, whose width  $W2$  is  $340\text{ }\mu\text{m}$  and whose thickness is  $15\text{ }\mu\text{m}$  at the central portion and  $5\text{ }\mu\text{m}$  at the peripheral portions with respect to a pressure producing chamber having a width  $W1$  of  $420\text{ }\mu\text{m}$ , is formed, and then a piezoelectric vibrating element 23, whose width  $W3$  is  $380\text{ }\mu\text{m}$ , and whose thickness is  $30\text{ }\mu\text{m}$  is formed on the surface of the drive electrode 21.

The thus constructed ink jet recording head and an ink jet recording head in which the drive electrodes are uniformly 5  $\mu\text{m}$  thick were compared. The amount of displacement of the piezoelectric vibrating element toward the pressure producing chamber is 0.2  $\mu\text{m}$  in the former, whereas such amount is 0.1  $\mu\text{m}$  in the latter. Therefore, an improvement that doubles the conventional amount of displacement was verified. The crosstalk of the former is 10% or less, whereas that of the latter from 30 to 60%. Therefore, a reduction of 1/3 or less in crosstalk was achieved.

In a manner similar to the above-mentioned embodiment, to improve displacement efficiency of the vibrating plate 3, i.e., the ratio of the applied electric energy to the ink removing volume, it is preferable to adjust the ratio of the width  $W1$  of the pressure producing chamber 5 to the width  $W2$  of the drive electrode 21,  $W2/W1$ , which is ideally set to 0.9, to a value between 0.8 and 0.9 considering errors and variations in the manufacturing process. Further, the thickness of the drive electrode 21 at the central portion is set to a value 1.2 or more times the thickness thereof at the peripheral portions. It has been verified that such setting contributes to preventing the reduction in yield due to errors and the like in the manufacturing process with certainty.

A method of manufacturing the thus constructed ink jet recording head will be described next with reference to Figures 14(a) to (f).

The vibrating plate 3, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6 are formed of green sheets, each green sheet being a ceramic material, i.e., a clay-like sheet and the pressure producing chamber forming member 4 having windows formed at regions designed to serve as the pressure producing chambers 5 by punching; and pressure is applied to the green sheets with these members half-solidified so that these members are integrated with one another, Figure 14(a). Then, the thus processed body is baked at temperatures ranging from 800 to 1500°C, Figure 14(b). The ceramic material generally consists essentially of one kind or more of compound selected from the group consisting of aluminum oxide, zirconium oxide, magnesium oxide, aluminum nitride, and silicon nitride.

When the vibrating plate 3, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6 have been integrated in this way, a pattern of the drive electrode 21 having an optimal width with respect to the corresponding pressure producing chamber 5 is formed by coating or printing an electrically conducting material to a region corresponding to the pressure producing chamber 5 of the vibrating plate 3 so that the ratio of the width  $W_2$  of the drive electrode 21 to the width  $W_1$  of the pressure producing chamber 5,  $W_2/W_1$ , is set to a value between 0.8 and 0.9. The electrically conducting material consists essentially of one kind or more of alloy selected from the group consisting of platinum, palladium, silver-palladium, silver-platinum, and platinum-palladium. Since the drive electrode 21 must be made arcuate in section in this embodiment, a first layer 21-1 is coated to a predetermined thickness and a second layer 21-2 is thereafter coated only in the vicinity of the center. This coating technique allows the electrically conducting material of which the second layer 21-2 is made to smoothly spread with the central portion thereof as the apex while promoted by the fluidity of the material of which the electrode is made, so that the second layer 21-2 is fused with the first layer 21-1 to be integrated therewith to have an arcuate section, in Figure 14 (c).

After the pattern of the drive electrode 21 has been half-solidified on the vibrating plate 3, the whole body is baked at a temperature suitable for baking the electrically conducting material, in Figure 14(d).

Then, the piezoelectric vibrating element 23 is formed on the surface of the drive electrode 21 by coating or printing a green sheet consisting of a piezoelectric material so that the width of the piezoelectric vibrating element 23 is larger than the width of the drive electrode 21 formed on the surface of the vibrating plate 3 and smaller than the width of the pressure producing chamber 5, in Figure 14(e). The piezoelectric material consists essentially of lead zirconate titanate, lead magnesium-niobate, lead nickel-niobate, lead zinc-niobate, lead manganese-niobate, lead antimony-stannate, or lead titanate.

When the green sheet, which is a piezoelectric material and which has been formed so as to be slightly projected from the drive electrode 21, has been half-solidified in this way, the whole body is baked at a temperature suitable for baking the piezoelectric material, in Figure 14(f).

In this baking process the central portion of the vibrating plate 3 flexes toward the pressure producing chamber 5 due to the rate of contraction of the piezoelectric vibrating element 23 at the time of baking being larger than that of the drive electrode 21 and due to contraction on the outer side of the piezoelectric vibrating element 23 being larger than contraction on the drive electrode 21 side of the piezoelectric vibrating element 23. However, since the central portion of the drive electrode 21 which has been formed thicker in advance fills the space formed by the flexion, the surface of the drive electrode 21 can be made horizontal.

When the electrode layer is formed by coating, the thickness of the layer usually includes about 20% of inconsistency. Therefore, it is preferable to make the central portion 1.2 or more times thicker than the peripheral portion, taking the safety factor into consideration. This technique is quite helpful in improving yield.

As the piezoelectric vibrating element baking process has been completed in this way, the common electrode 80 is formed by depositing an electrically conducting material, e.g., copper or nickel, using a mask having a window covering the surfaces of all the piezoelectric vibrating elements 23, as shown in Figure 7.

If necessary, a thin electrically insulating layer <sup>81</sup> is used to fill regions of the vibrating plate 3 where no piezoelectric vibrating element 23 is formed so that the layer <sup>81</sup> becomes as high as the piezoelectric vibrating element 23 as shown in Figure 15, and the common electrode 80 is deposited thereon, so that not only generation of crosstalk due to signal leakage can be prevented by securing electric insulation between the adjacent drive electrodes 21, but also breakage of the common electrode 80 at the ends of the piezoelectric vibrating element 23 can be prevented by making the step between the piezoelectric vibrating element 23 and the vibrating plate 3 small.

Figure 16 shows another embodiment. An electrode 24 formed so as to confront the pressure producing chamber 5 is similarly made arcuate in section at a region confronting the pressure producing chamber 5. On the other hand, a region 24a that extends uniformly at such a thickness as to ensure electric conduction is formed at other regions. This region 24a is connected to an electrode 24' formed on an adjacent pressure producing chamber 5. That is, the electrodes that serve to select the piezoelectric vibrating elements 23 for driving in the above-mentioned embodiments are used as the common electrodes, and drive electrodes 83, 83' that are electrically independent of the piezoelectric vibrating elements 23, 23' are formed on the surfaces of the respective piezoelectric vibrating elements 23, 23'.

While the surface of the drive electrode is made flat by filling the recess formed by the flexion of the vibrating plate 3 with the electrically conducting material, a similar effect can be obtained by using other materials.

Figure 17 shows still another embodiment of the invention. A third layer 30 is formed and a drive electrode 31 is formed thereon. The third layer 30 is made of a material which is other than the piezoelectric material and which has strong adhesion with respect to both the vibrating plate 3 and the electrode. The third layer 30 is formed so as to be arcuate in section so that the central portion of the vibrating plate 3 confronting the pressure producing chambers is thick with a smoothly thinning slope toward the peripheral portions. The drive electrode 31 corrects the flexion of the vibrating plate 3, and similarly has a narrower width than the pressure producing chamber and a uniform thickness.

Also in this embodiment, the piezoelectric vibrating element 32 is formed so as to be substantially horizontal at a level higher than the vibrating plate 3. Therefore, generation of crosstalk and reduction in ink expelling efficiency can be prevented.

Figures 18(a) to (h) show a method of manufacturing the above-mentioned recording head, the method being an embodiment of the invention. Pressure is applied to the vibrating plate 3, the pressure producing chamber forming member 4, and the pressure producing chamber forming cover member 6, which are in the form of green

sheets, and integrally baked at temperatures ranging from 800 to 1500°C, in Figure 18 (a) and (b). The pressure producing chamber forming member 4 has portions designed to serve as the pressure producing chambers 5 formed by punching. Each green sheet is a ceramic such as alumina or zirconia.

The third layer 30 that is thicker at the central portion than the peripheral portion is formed at a region corresponding to the pressure producing chamber 5 by printing, in Figure 18(c) and baked, in Figure 18(d). The third layer 30 is made of a material which is other than the piezoelectric material and which has adhesion with respect to both the vibrating plate 3 and the electrode 31, e.g., ceramic or metal.

In these processes, it is similarly preferable to form the central portion 1.2 times thicker than the peripheral portions, taking errors in the manufacturing process into account.

Then, the material of which the electrode 31 is made is deposited on the surface of the third layer 30 so as to confront the pressure producing chamber 5 by printing, in Figure 14(e), and baked, in Figure 18(f).

As the final process, the piezoelectric vibrating element 32 is similarly formed by printing, in Figure 18(g), and baked, in Figure 18(h).

According to this embodiment, freedom in selecting the material used to compensate for the deformation of the vibrating plate 3 is increased, thereby allowing the vibrating characteristic of the vibrating plate 3 to be adjusted to a value optimal for ink expelling.

### CLAIMS:

1. An ink jet recording head comprising:

a plurality of chambers for retaining ink, each chamber having a length and width;

a vibrating plate disposed on a surface of the chambers;

a plurality of electrodes disposed on the vibrating plate, each electrode corresponding to a respective chamber;

a plurality of piezoelectric elements disposed on the electrodes, each piezoelectric element corresponding to a respective electrode and chamber

a common electrode disposed on the plurality of piezoelectric elements and providing an electric connection with each electrode at one end of the length of each chamber such that applying a drive signal across the common electrode and a selected electrode leads to flexing of the respective piezoelectric element which applies pressure to the respective chamber for expelling a drop of ink therefrom;

wherein at least the vibrating plate and chambers are formed from a ceramic and bonded together by baking,

each piezoelectric element is disposed to cover completely the width of the respective electrode,

and a peripheral edge of each piezoelectric vibrating element is formed as an overhang with respect to the electrode and is attached to the vibrating plate via the electrode.

2. An ink jet recording head as claimed in claim 1, in which a width W2 of each electrode is smaller than a width W1 of the respective chamber, and a width W3 of the respective piezoelectric vibrating element is larger than the width W2 of the electrode and smaller than the width W1 of the chamber.

3. An ink jet recording head according to claim 1 or 2, wherein a ratio of the width W2 of the electrode to the width W1 of the chamber,  $W2/W1$ , is set to a value between 0.8 and 0.9.
4. An ink jet recording head according to claim 1, wherein an electrically insulating layer is formed between the electrodes.
5. An ink jet recording head comprising:
- a vibrating plate made of ceramic; a pressure producing chamber forming member, made of ceramic, for forming a plurality of pressure producing chambers in rows; an electrode on one pole formed on a surface of the vibrating plate so as to correspond to the pressure producing chamber;
  - a piezo electric vibrating element, one end thereof contacting the electrode and other end thereof contacting an electrode on other pole, the ink jet recording head expelling an ink droplet from a nozzle opening by flexion of the piezoelectric vibrating element; and
  - a member through which the piezoelectric vibrating element is fixed to the vibrating plate, the member shaped in arcuate in section, a central portion of the member which confronts the pressure producing chamber of the vibrating plate being larger in thickness than a peripheral edge of the member, the member projected toward a pressure producing chamber side,
- wherein at least the vibrating plate and the pressure producing chamber forming member are integrally formed by baking the ceramic, the piezoelectric vibrating element is deposited by baking on the surface of the electrode on the one pole formed on the surface of the vibrating plate.

6. An ink jet recording head according to claim 5, wherein the member is made of a material having an adhesive force with respect to both the piezoelectric vibrating element and the vibrating plate without a piezoelectric property.
7. An ink jet recording head according to claim 5, wherein the member is the electrode on the one pole.
8. An ink jet recording head according to claim 5, wherein a ratio in thickness of the central portion of the member to the peripheral edge portion thereof is 1.2 or more.
9. An ink jet recording head according to claim 5, wherein a width W2 of the electrode on the one pole is smaller than a width W1 of the pressure producing chamber, and a width W3 of the piezoelectric vibrating element is larger than the width W2 of the electrode on the one pole and is smaller than the width W1 of the pressure producing chamber.
10. An ink jet recording head according to claim 5, wherein a ratio of the width W2 of the electrode on the one pole to the width W1 of the pressure producing chamber,  $W2/W1$ , is set to a value between 0.8 and 0.9.
11. An ink jet recording head according to claim 5, wherein the electrode on the one pole is a drive electrode and the electrode on the other pole is a common electrode.
12. An ink jet recording head according to claim 5, wherein the peripheral edge of the piezoelectric vibrating element is formed to an overhang with respect to the electrode on the one pole and is substantially fixed to the vibrating plate through the electrode on the one pole.

13. An ink jet recording head according to claim 5, wherein an electrically insulating layer is formed between the electrodes on the one pole.

14. A method of manufacturing an ink jet recording head comprising the steps of:  
forming a vibrating plate, a pressure producing chamber forming member, and a pressure producing chamber forming cover member of green sheets, respectively, the pressure producing chamber forming member having windows formed at regions designed to serve as pressure producing chambers by punching, each green sheet being a ceramic material including alumina or zirconia;

applying pressure with the vibrating plate to the pressure producing chamber forming member and the pressure producing chamber forming cover member when half-solidified, so as to integrate the members with each other to form a processed body;

baking the processed body;

forming a pattern of an electrode on one pole of an electrically conducting material on an upper surface of the vibrating plate at a region corresponding to a pressure producing chamber of the vibrating plate so that a ratio of a width  $W_2$  of the electrode on the one pole to a width  $W_1$  of the pressure producing chamber,  $W_2/W_1$ , is set to a value between 0.8 and 0.9;

when the pattern of the electrode on the one pole of the vibrating plate has been half-solidified, baking the thus resulted whole at a temperature suitable for baking the electrically conducting material; and

forming a layer of a piezo-electric material of width  $W_3$  on an upper surface of the electrode so as to be wider than the width  $W_2$  of the electrode on the one pole and narrower than the width  $W_1$  of the pressure producing chamber, and baking the whole body.

15. A method of manufacturing an ink jet recording head according to claim 14, wherein the ceramic material is one kind or more of compound selected from the group consisting of aluminium oxide, zirconium oxide, magnesium oxide, aluminium nitride, and silicon nitride, and the piezoelectric material consists essentially of lead zirconate titanate, lead magnesium-niobate, lead nickel-niobate, lead manganese-niobate, lead antimony-stannate, and lead titanate, and the electrically conducting material consists essentially of one kind or more of alloy selected from the group consisting of platinum, palladium, silver-palladium, silver-platinum, and platinum-palladium.

16. A method of manufacturing an ink jet recording head comprising the steps of:  
forming a vibrating plate, a pressure producing chamber forming member, and a pressure producing chamber forming cover member of green sheets, respectively, the pressure producing chamber forming member having windows formed at regions designed to serve as pressure producing chambers by punching, each green sheet being a ceramic material including alumina or zirconia;

applying pressure with the vibrating plate to the pressure producing chamber forming member, and the pressure producing chamber forming cover member when half-solidified, so as to integrate the members with each other to form a processed body;

baking the processed body;

forming a pattern of an electrode on one pole of an electrically conducting material on an upper surface of the vibrating plate at a region corresponding to a pressure producing chamber of the vibrating plate so that a ratio of a width  $W_2$  of the electrode on the one pole to a width  $W_1$  of the pressure producing chamber,  $W_2/W_1$ , is set to a value between 0.8 and 0.9 and so that a central portion of the electrode on the one pole is arcuate in section;

when the pattern of the electrode on the one pole of the vibrating plate has been half-solidified, baking the thus resulted whole at a temperature suitable for baking the electrically conducting material; and

forming a layer of a piezoelectric material of width W3 on an upper surface of the electrode so as to be wider than the width W2 of the electrode on the one pole and narrower than the width W1 of the pressure producing chamber, and baking the whole body.

17. A method of manufacturing an ink jet recording head according to claim 16, wherein the electrode on the one pole is formed a plurality of times so that the central portion thereof becomes arcuate in section.

18. A method of manufacturing an ink jet recording head comprising the steps of:  
forming a vibrating plate, a pressure producing chamber forming member, and a pressure producing chamber forming cover member of green sheets, respectively, the pressure producing chamber forming member having windows formed at regions designed to serve as pressure producing chambers by punching, each green sheet being a ceramic material including alumina or zirconia;

applying pressure with the vibrating plate to the pressure producing chamber forming member and the pressure producing chamber forming cover member when half-solidified, so as to integrate the members with each other to form a processed body;

baking the processed body;

printing a layer of a material, the material having an adhesive force with respect to the vibrating plate and an electrode on one pole, on an upper surface of the vibrating plate at a region corresponding to the pressure producing chamber of the vibrating plate so that a central portion of the layer becomes arcuate in section;

baking the body;

forming a pattern of the electrode on the one pole of an electrically conducting material on an upper surface of the layer so that a ratio of a width W2 of the electrode

on the one pole to a width W1 of the pressure producing chamber,  $W2/W1$ , is set to a value between 0.8 and 0.9;

baking the thus resulted whole at a temperature suitable for baking the electrically conducting material when the pattern of the electrode on the one pole of the vibrating plate has been half-solidified; and

forming a layer of a piezoelectric material so as to be wider than the width W2 of the electrode on the one pole and narrower than the width W1 of the pressure producing chamber, and baking the layer.

19. A method of manufacturing an ink jet recording head according to claim 16, wherein the ceramic material is one kind or more of compound selected from the group consisting of aluminum oxide, zirconium oxide, magnesium oxide, aluminum nitride, and silicon nitride; the piezoelectric material consists essentially of lead zirconate titanate, lead magnesium-niobate, lead nickel-niobate, lead manganese-niobate, lead antimony-stannate, or lead titanate; and the electrically conducting material consists essentially of at least one kind or more of alloy selected from the group consisting of platinum, palladium, silver-palladium, silver-platinum, and platinum-palladium.

20. A method of manufacturing an ink jet recording head according to claim 18, wherein the ceramic is one kind or more of compound selected from the group consisting of aluminum oxide, zirconium oxide, magnesium oxide, aluminum nitride, and silicon nitride; the piezoelectric material consists essentially of lead zirconate titanate, lead magnesium-niobate, lead nickel-niobate, lead manganese-niobate, lead antimony-stannate, or lead titanate; and the electrically conducting material consists essentially of at least one kind or more of alloy selected from the group consisting of platinum, palladium, silver-palladium, silver-platinum, and platinum-palladium.

21. An ink jet recording head comprising:
- a plurality of chambers for retaining ink, each chamber having a length and width;
  - a vibrating plate disposed on a surface of the chambers;
  - a first electrode disposed on the vibrating plate in a position corresponding to at least one of the chambers;
  - a piezoelectric element disposed on the electrode;
  - a second electrode disposed on the piezoelectric element;
- wherein the piezoelectric element is disposed to cover completely the width of the first electrode,
- and a peripheral edge of the piezoelectric vibrating element is formed as an overhang with respect to the electrode and is attached to the vibrating plate via the electrode.
22. An ink jet recording head as claimed in claim 21, in which a width W2 of the first electrode is smaller than a width W1 of the chamber, and a width W3 of the piezoelectric vibrating element is larger than the width W2 of the first electrode and smaller than the width W1 of the chamber.
23. An ink jet recording head according to claim 21 or 22, wherein a ratio of the width W2 of the first electrode to the width W1 of the chamber,  $W2/W1$ , is set to a value between 0.8 and 0.9.
24. An ink jet recording head according to claim 21, wherein an electrically insulating layer is formed between the first electrode.

25. An ink jet recording head comprising:

a vibrating plate; a pressure producing chamber forming member, for forming a plurality of pressure producing chambers in rows; a first electrode formed on a surface of the vibrating plate so as to correspond to the pressure producing chamber;

a piezo electric vibrating element, one end thereof contacting the first electrode and other end thereof contacting a second electrode, the ink jet recording head expelling an ink droplet from a nozzle opening by flexion of the piezoelectric vibrating element; and

a member through which the piezoelectric vibrating element is fixed to the vibrating plate, the member shaped in arcuate in section, a central portion of the member, which confronts the pressure producing chamber of the vibrating plate being larger in thickness than a peripheral edge of the member, the member projected toward a pressure producing chamber side.

26. An ink jet recording head according to claim 25, wherein the member is made of a material having an adhesive force with respect to both the piezoelectric vibrating element and the vibrating plate without a piezoelectric property.

27. An ink jet recording head according to claim 25, wherein the member is the first electrode.

28. An ink jet recording head according to claim 25, wherein a ratio in thickness of the central portion of the member to the peripheral edge portion thereof is 1.2 or more.

29. An ink jet recording head according to claim 25, wherein a width W2 of the first electrode is smaller than a width W1 of the pressure producing chamber, and a width W3 of the piezoelectric vibrating element is larger than the width W2 of the first electrode and is smaller than the width W1 of the pressure producing chamber.

30. An ink jet recording head according to claim 25, wherein a ratio of the width W2 of the first electrode to the width W1 of the pressure producing chamber,  $W2/W1$ , is set to a value between 0.8 and 0.9.
31. An ink jet recording head according to claim 25, wherein the first electrode is a drive electrode and the second electrode is a common electrode.
32. An ink jet recording head according to claim 25, wherein the peripheral edge of the piezoelectric vibrating element is formed to an overhang with respect to the first electrode and is substantially fixed to the vibrating plate through the first electrode.
33. An ink jet recording head according to claim 25, wherein an electrically insulating layer is formed between the first electrode.
34. An ink jet recording head substantially as hereinbefore described with reference to and/or as illustrated in any one of accompanying Figures 1 to 5, 7 to 11.
35. A method of manufacturing an ink jet recording head substantially as hereinbefore described with reference to and/or as illustrated in any one of accompanying Figures 6(a) to 6(f), 14(a) to 14(f).

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